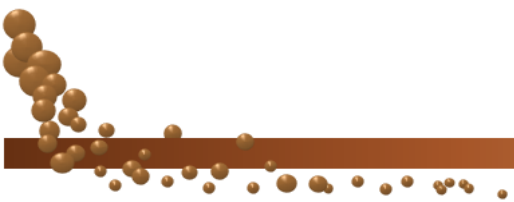


LECTURE 4

FET Circuits



DISCRETE COMPONENT FET

FET (Field-Effect Transistor)

JFET (Junction Field-Effect Transistor)

MOSFET (Metal-Oxide_Semiconductor FET)

Depletion-mode

Depletion-mode

Enhancement-mode

N-channel

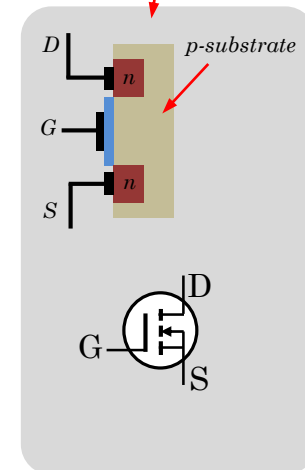
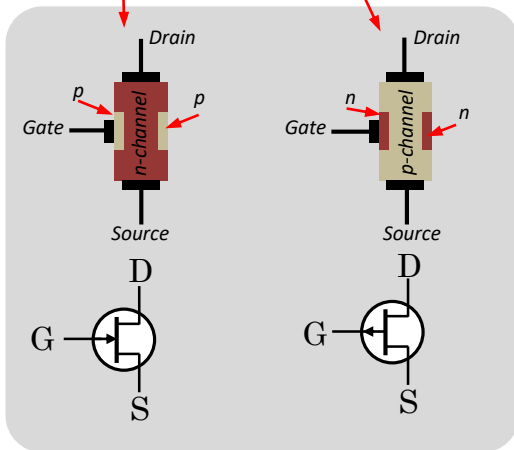
P-channel

N-channel

P-channel

N-channel

P-channel



DISCRETE COMPONENT FET

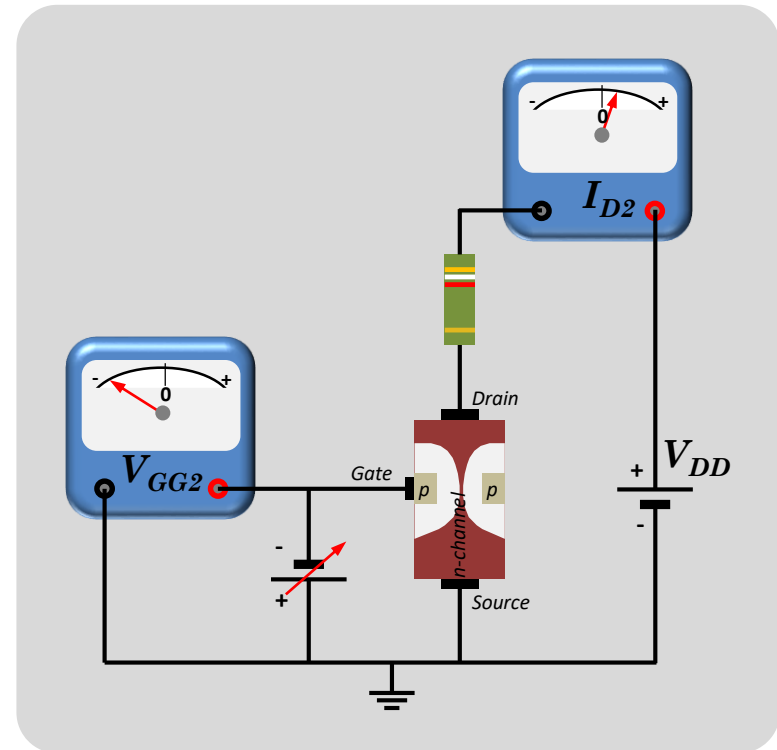
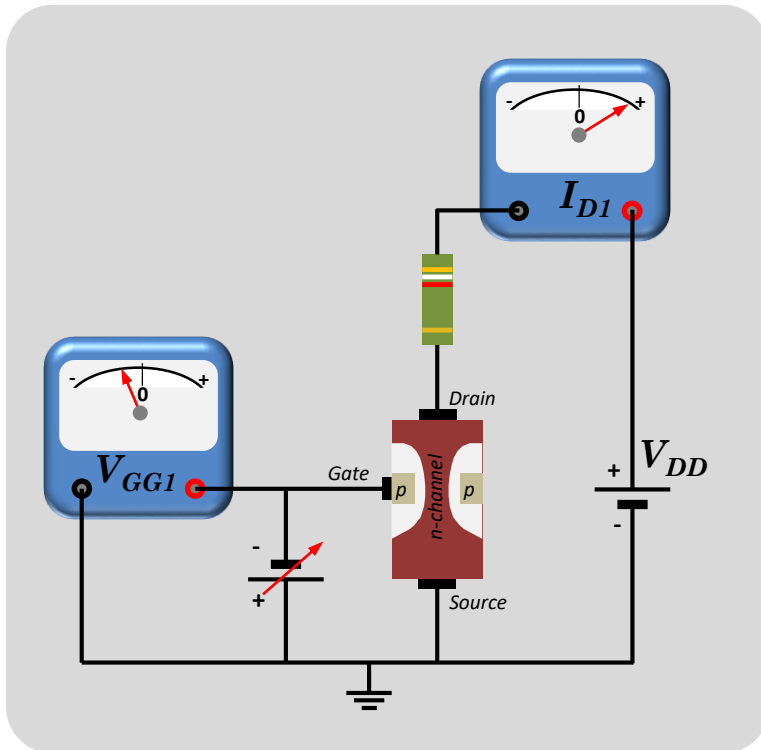
Symbols in FET-amplifiers

	Supply	Quisient	ac instant	ac rms	ac+dc instant	ac+dc average
Drain voltage	V_{DD}	V_{DQ}	v_d	V_d	v_D	V_D
Drain current	I_{DD}	I_{DQ}	i_d	I_d	i_D	I_D
Gate voltage	V_{GG}	V_{GQ}	v_g	V_g	v_G	V_G
Gate current	I_{GG}	I_{GQ}	i_g	I_g	i_G	I_G
Source voltage	V_{SS}	V_{SQ}	v_s	V_s	v_S	V_S
Source current	I_{SS}	I_{SQ}	i_s	I_s	i_S	I_S

A biased n-channel JFET

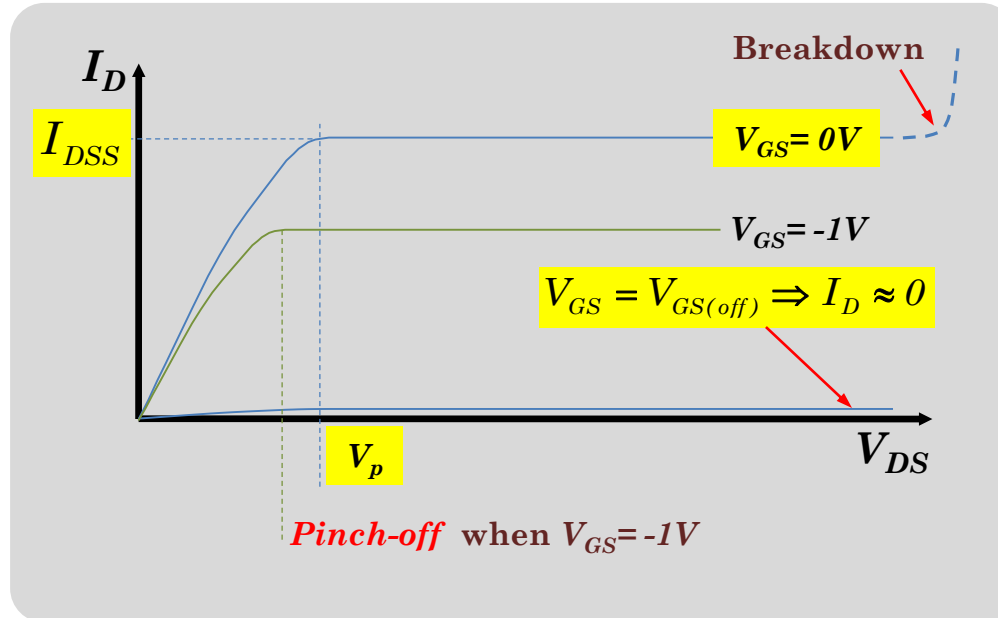
Large signal analysis

$$|V_{GG2}| > |V_{GG1}| \Rightarrow I_{D2} < I_{D1}$$



A biased n-channel JFET

Large signal analysis



Drain Characteristic Curve

Cutoff voltage $V_{GS(off)}$

Pinch-off voltage V_p when $V_{GS} = 0$

Breakdown

Input range for V_{GS} when $V_{DS} > V_p$

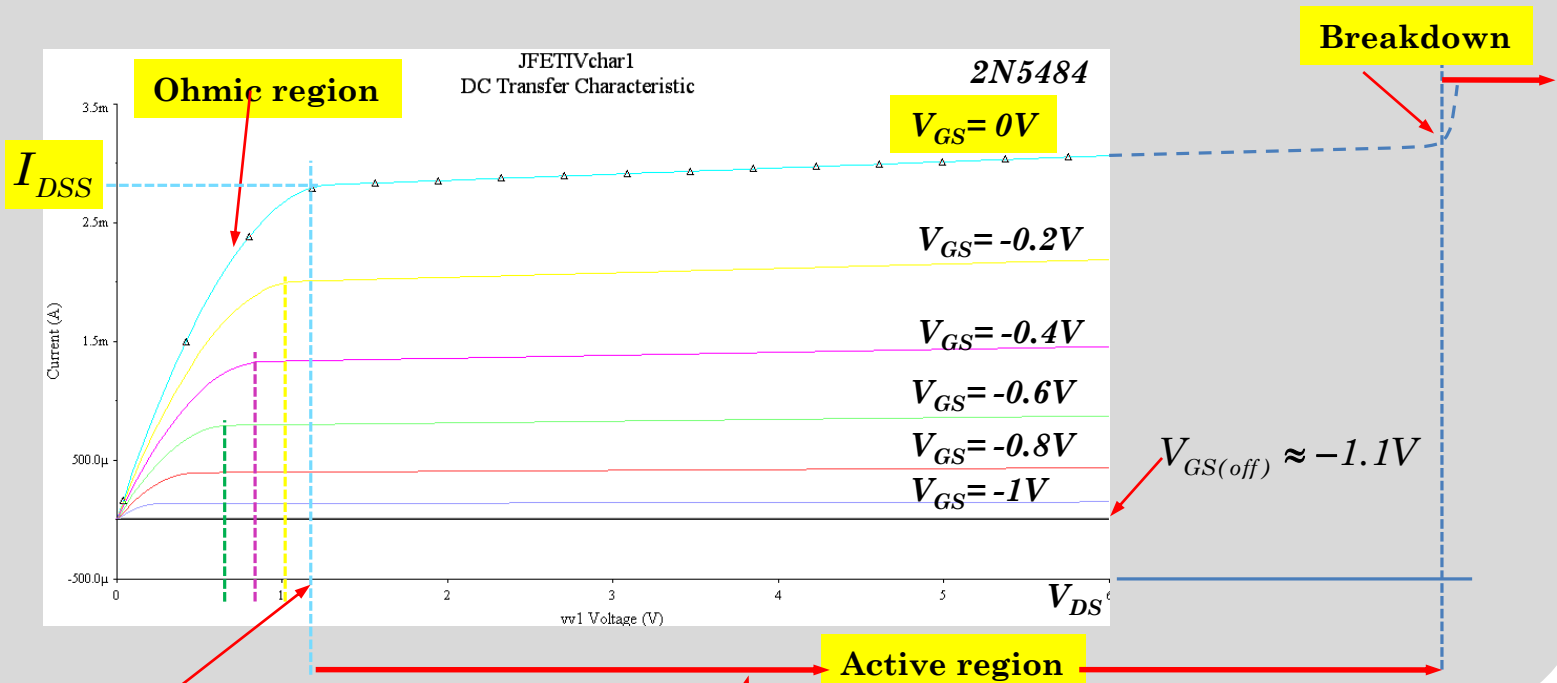
$$V_{GS(off)} < V_{GS} < 0 \quad \Rightarrow \quad 0 < I_D < I_{DSS}$$

$$-|V_{GS(off)}| = |V_p|$$

A biased n-channel JFET

Large signal analysis
Example of typical rf JFET 2N5484

Family of drain characteristic curves for 2N5484



Pinch-off voltage V_p
Assumption: $V_{GS} = 0V$

Active operation region

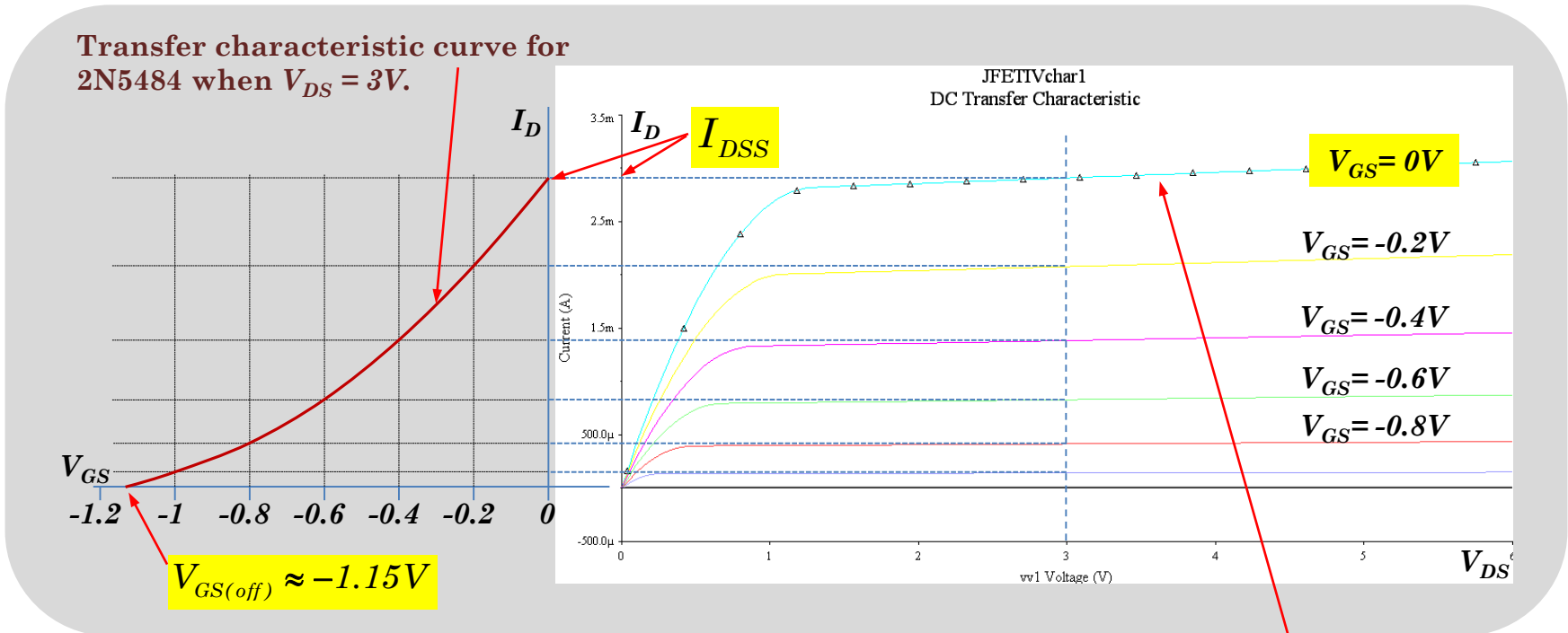
Data sheet of 2N5484

A biased n-channel JFET

Active region

Large signal analysis

Example of typical rf JFET 2N5484

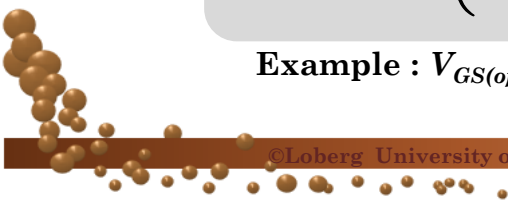


$$I_D \cong I_{DSS} \left(1 - \frac{V_{GS}}{V_{GS(off)}} \right)^2$$

Example : $V_{GS(off)} = -1.15V$ and $-1V < V_{GS} < 0$

Approximation

The slope of drain characteristic in active region is zero.



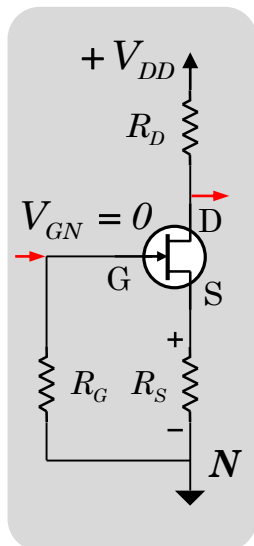
A biased n-channel JFET

Active region

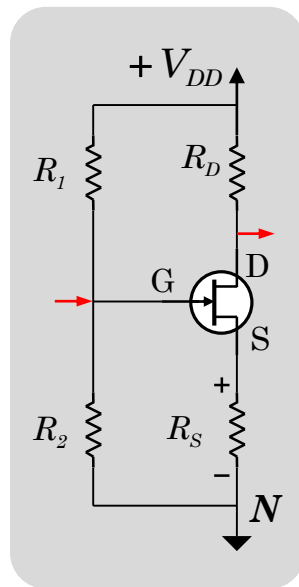
Large signal analysis

The four basic biasing schemes

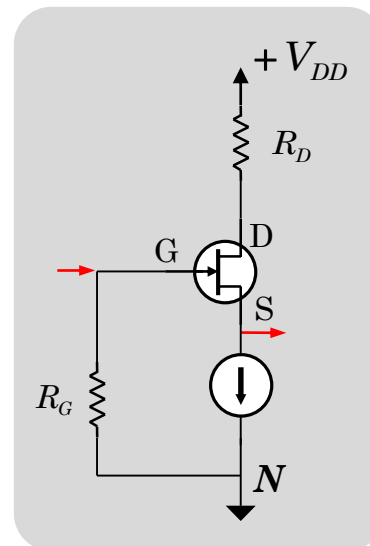
Self bias



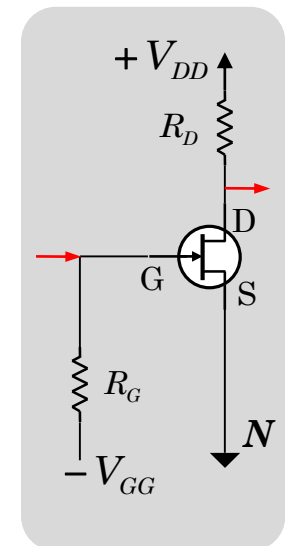
Voltage-divider bias



Constant current-source bias



Constant voltage bias



A biased n-channel JFET SELF-BIAS

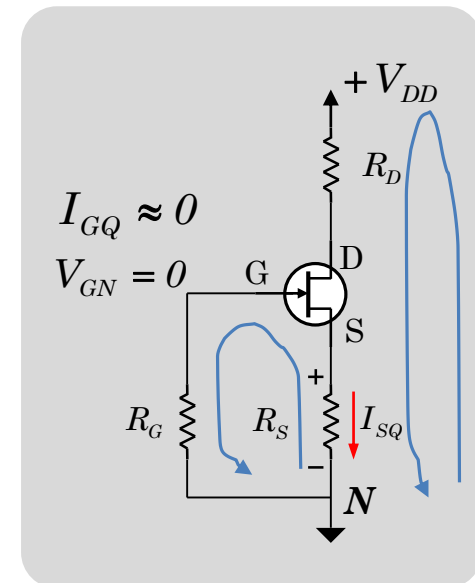
Active region

Large signal analysis

$$I_{SQ}R_S + V_{GSQ} + 0 = 0$$

$$V_{DD} - I_{DQ}R_D - V_{DSQ} - I_{SQ}R_S = 0$$

$$I_{SQ} = I_{DQ}$$



$$V_{GSQ} = -I_{DQ}R_S$$

$$V_{DSQ} = V_{DD} - I_{DQ}(R_D + R_S)$$

A biased n-channel JFET SELF-BIAS

If we know parameters $V_{GS(off)}$ and I_{DSS} , we can solve V_{GSQ} by using the following equation.

$$I_{DQ} \cong I_{DSS} \left(1 - \frac{V_{GSQ}}{V_{GS(off)}} \right)^2$$

Or graphical analysis : We can solve V_{GSQ} by using the transfer characteristic curve.

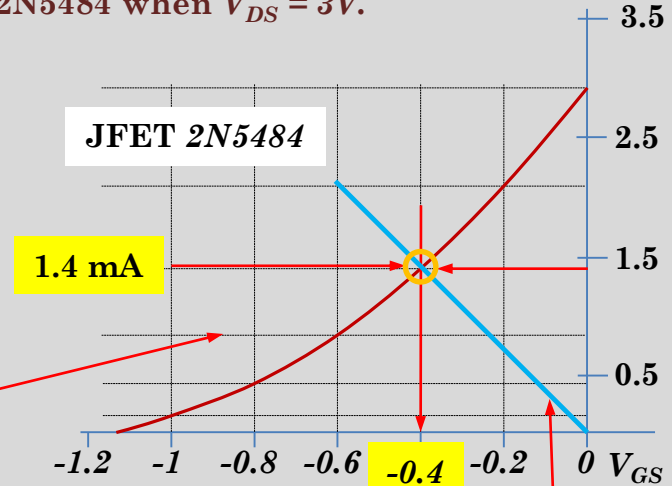
$$V_{GSQ} = -I_{DQ} R_S \Rightarrow R_S = -V_{GSQ} / I_{DQ}$$

$$R_D = \frac{V_{DD} - V_{DSQ}}{I_{DQ}} - R_S$$

Active region

Large signal analysis

Transfer characteristic curve for I_D [mA]
2N5484 when $V_{DS} = 3V$.



Self-bias dc LOAD LINE

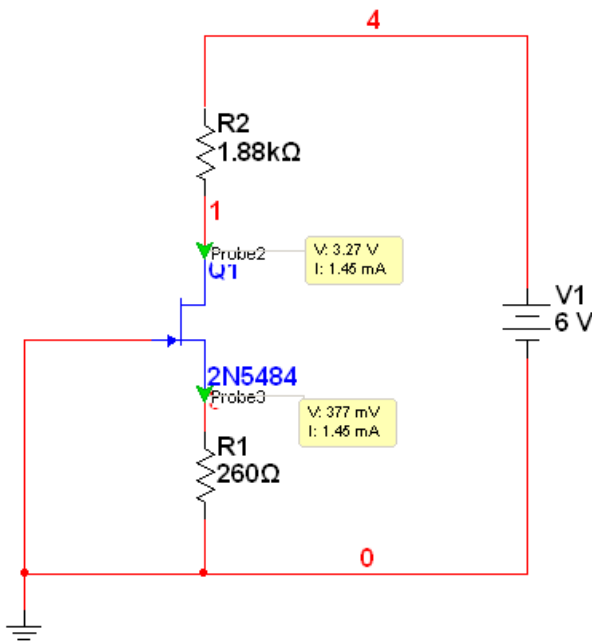
$$I_D = -\frac{1}{R_S} V_{GS}$$

A biased n-channel JFET SELF-BIAS EXAMPLE

Assumptions : $V_{DSQ} = 3V$

Typically $I_{DQ} \approx \frac{1}{2} I_{DSS} \approx 1.4 \text{ mA}$

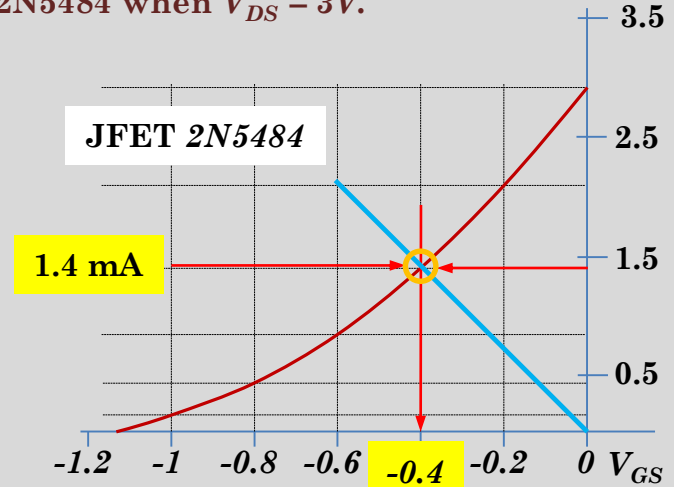
$V_{GS(off)} \approx -1.15V$ $I_{DSS} \approx 3 \text{ mA}$



Active region

Large signal analysis

Transfer characteristic curve for I_D [mA]
2N5484 when $V_{DS} = 3V$.



$$V_{GSQ} \approx 1.15V \left(\sqrt{\frac{1.4}{3}} - 1 \right) \approx -0.364V$$

$$R_S = -\frac{-0.364V}{1.4mA} = 260\Omega$$

$$R_D = \frac{6V - V_{DSQ}}{1.4mA} - 260\Omega = 1.9k\Omega$$

A biased n-channel JFET VOLTAGE-DIVIDER BIAS

$$V_{GN} = \left(\frac{R_2}{R_1 + R_2} \right) V_{DD}$$

$$V_{SN} = V_{GN} - V_{GS}$$

$$I_D = (V_{GN} - V_{GS}) / R_S$$

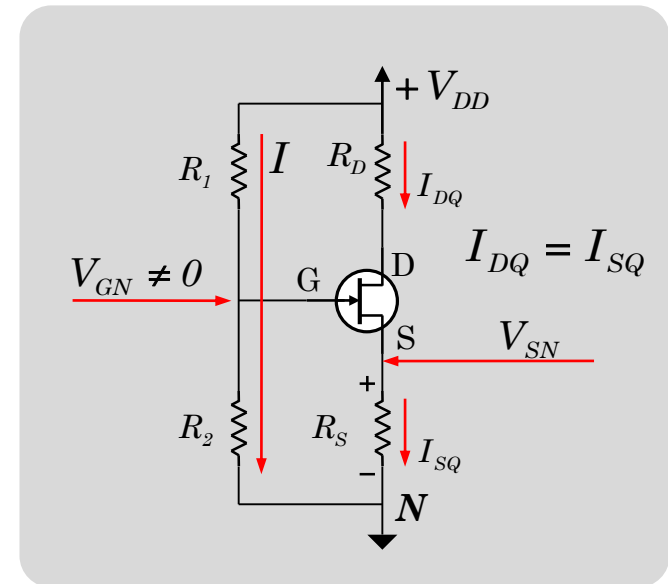
$$V_{DD} - V_{DS} - I_D (R_D + R_S) = 0$$

On biaspoint **Q**:
$$I_{DQ} \cong I_{DSS} \left(1 - \frac{V_{GSQ}}{V_{GS(off)}} \right)^2$$

$$V_{GSQ} = V_{GS(off)} \left(1 - \sqrt{\frac{I_{DQ}}{I_{DSS}}} \right)$$

Active region

Large signal analysis



$$I_D = \frac{1}{R_S} V_{GN} - \frac{1}{R_S} V_{GS}$$

Voltage-divider bias dc LOAD LINE

A biased n-channel JFET VOLTAGE-DIVIDER BIAS EXAMPLE

Active region

Large signal analysis

$$V_{GSQ} = V_{GS(off)} \left(1 - \sqrt{\frac{I_{DQ}}{I_{DSS}}} \right) \approx -0.364 V$$

$$I_{DQ} = (V_{GNQ} - V_{GSQ}) / R_S \Rightarrow V_{GNQ} = I_{DQ} R_S + V_{GSQ} = 1.036 V$$

$$V_{SNQ} = I_{DQ} R_S = 1.4 V$$

$$V_{GN} = \left(\frac{R_2}{R_1 + R_2} \right) V_{DD} \Rightarrow R_1 = R_2 \left(\frac{V_{DD} - V_{GNQ}}{V_{GNQ}} \right) = 1 M\Omega \frac{9V - 1.036 V}{1.036 V} = 7.68 M\Omega$$

$$V_{DD} - V_{DS} - I_D (R_D + R_S) = 0 \Rightarrow R_D = \frac{V_{DD} - V_{DSQ}}{I_{DQ}} - R_S = \frac{9V - 3V}{1.4 mA} - 1 k\Omega = 3.29 k\Omega$$

Assumptions : $V_{DSQ} = 3V$

Typically $I_{DQ} \approx \frac{1}{2} I_{DSS} \approx 1.4 mA$

$V_{GS(off)} \approx -1.15V$ $I_{DSS} \approx 3 mA$

$R_2 = 1 M\Omega$ $R_S = 1 k\Omega$

A biased n-channel JFET VOLTAGE-DIVIDER BIAS EXAMPLE

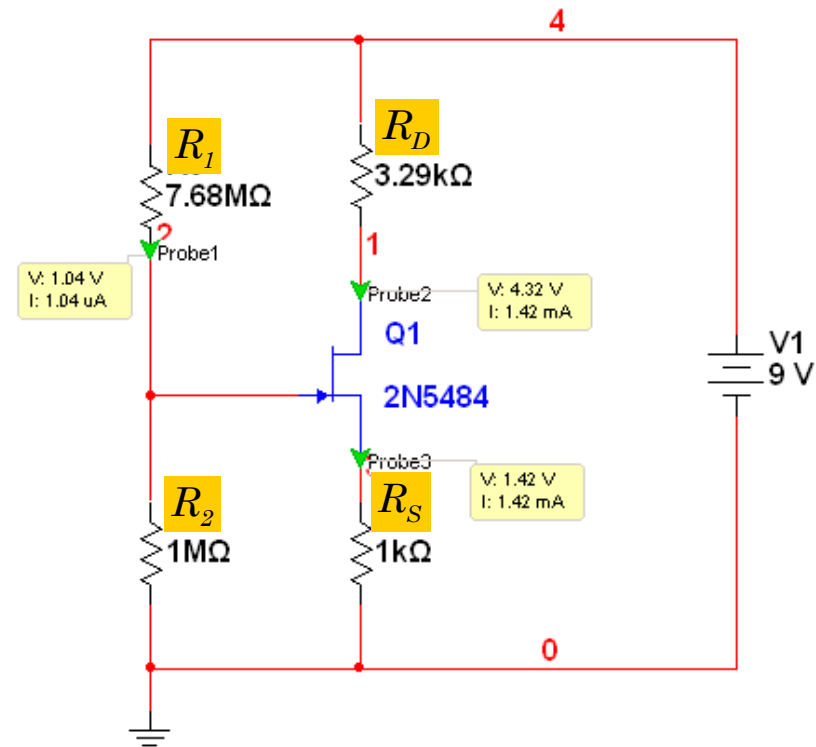
Active region

Large signal analysis

Assumptions : $I_{DQ} = 1.4\text{mA}$
 $V_{DSQ} = 3\text{V}$
 $R_2 = 1\text{M}\Omega$ $R_S = 1\text{k}\Omega$

Calculated values:
 $V_{GNQ} = 1.036\text{V}$
 $V_{SNQ} = 1.4\text{V}$
 $V_{GSQ} = -0.364\text{V}$
 $R_D = 3.29\text{k}\Omega$
 $R_1 = 7.68\text{M}\Omega$

Simulated bias point values

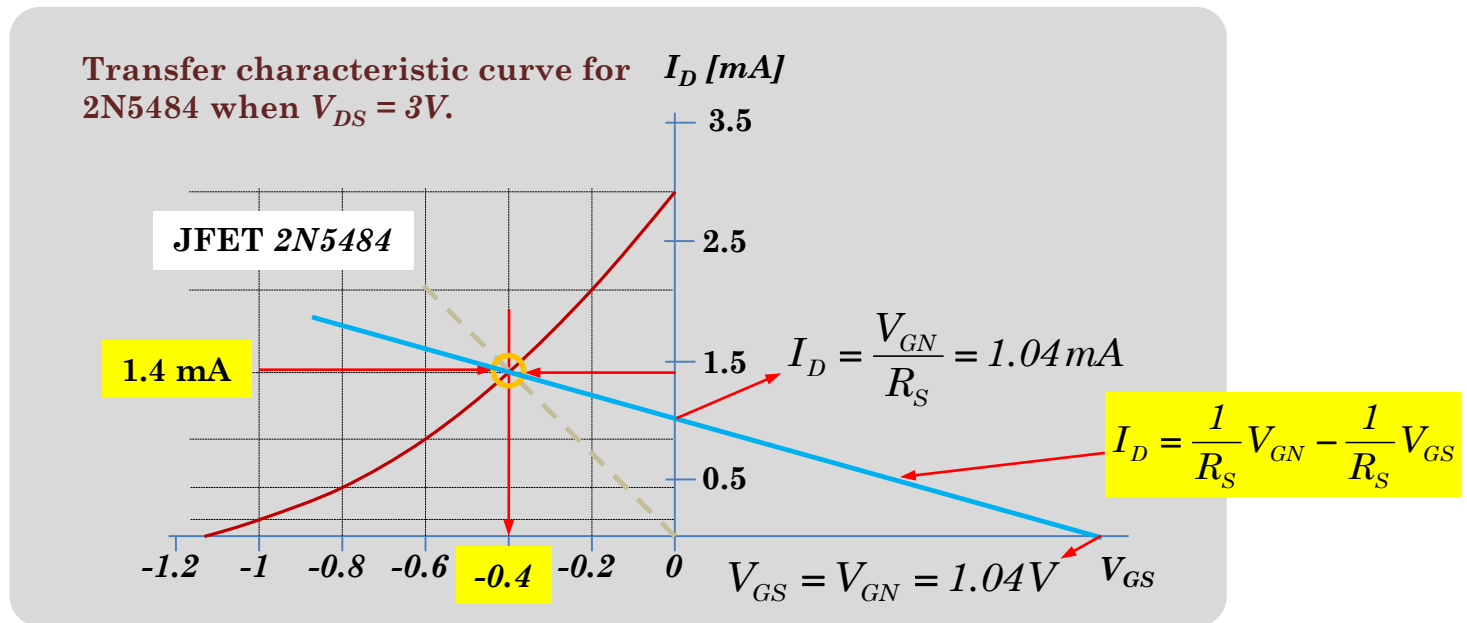


A biased n-channel JFET VOLTAGE-DIVIDER BIAS EXAMPLE

Active region

Large signal analysis

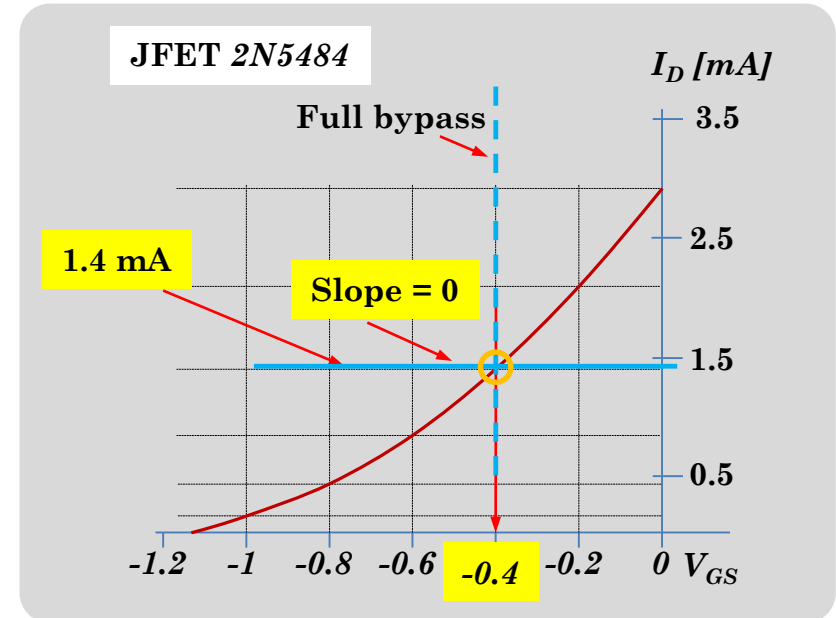
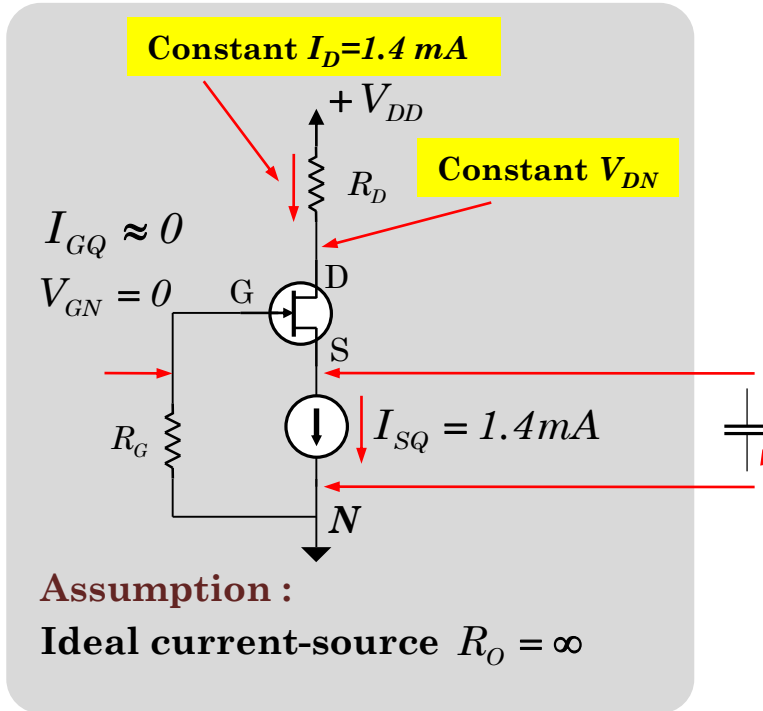
Graphical analysis



A biased n-channel JFET CONSTANT CURRENT-SOURCE BIAS

Active region

Large signal analysis



Limited to source follower type applications

Current-source must be bypassed with capacitor to get **drain** ac-signal.

A biased n-channel JFET CONSTANT CURRENT-SOURCE BIAS EXAMPLE

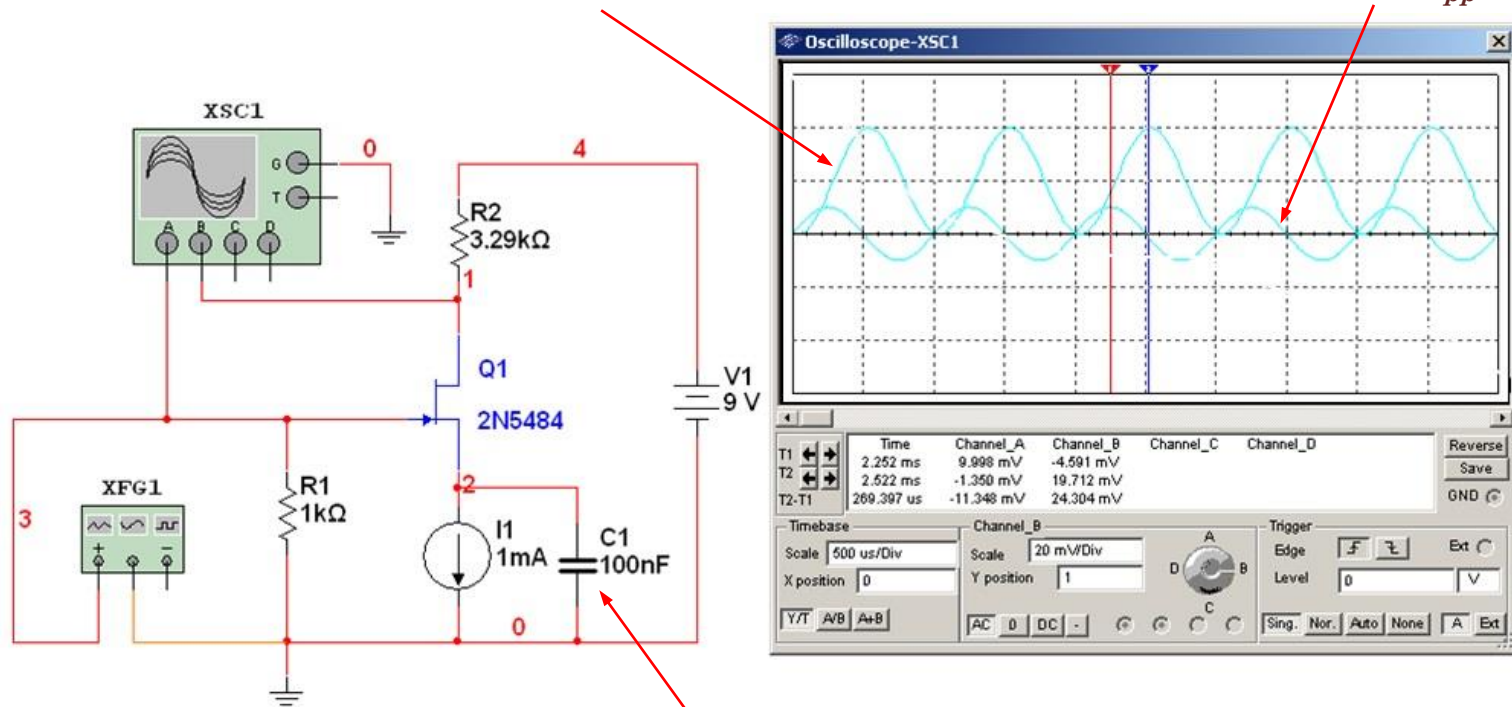
Active region

Large signal analysis

Simulation with BYPASS CAPACITOR

Output: DRAIN signal

Input: GATE ac-signal $V_{pp} = 20mV$



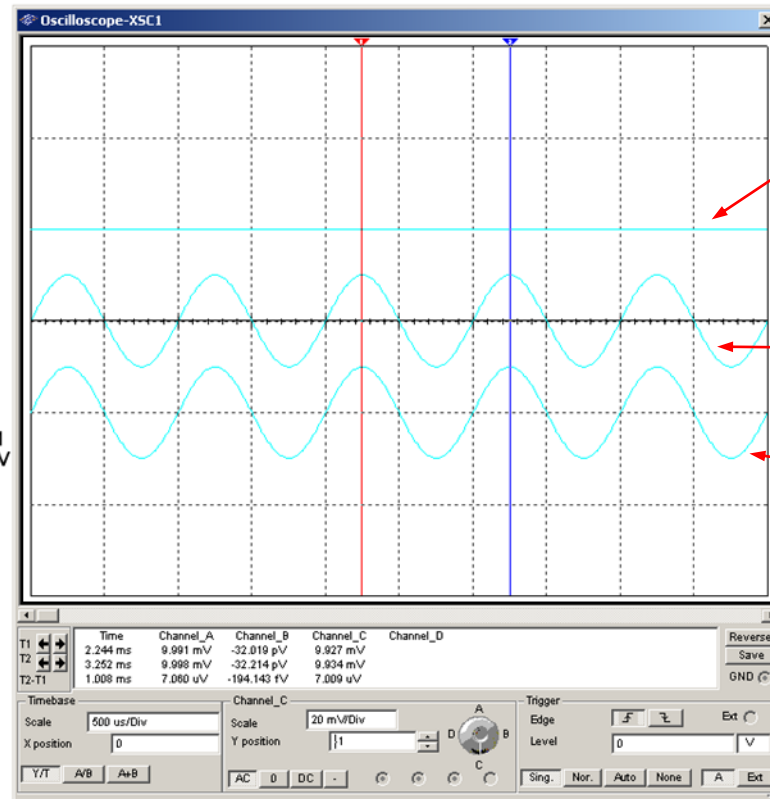
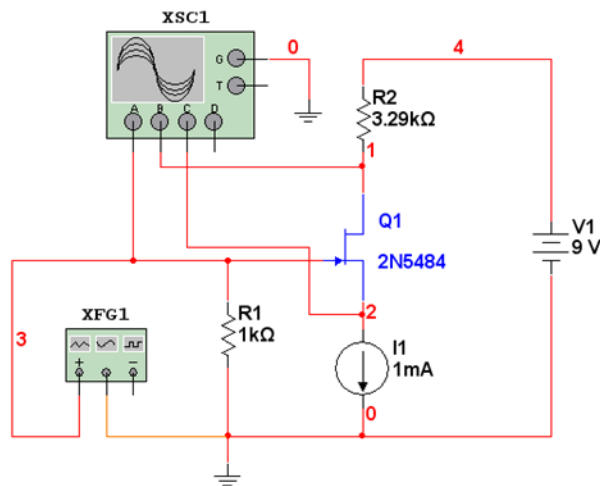
Bypass capacitor

A biased n-channel JFET CONSTANT CURRENT-SOURCE BIAS EXAMPLE

Active region

Large signal analysis

Simulation without BYPASS CAPACITOR



Output: DRAIN
ac-signal $V_{pp}=0$

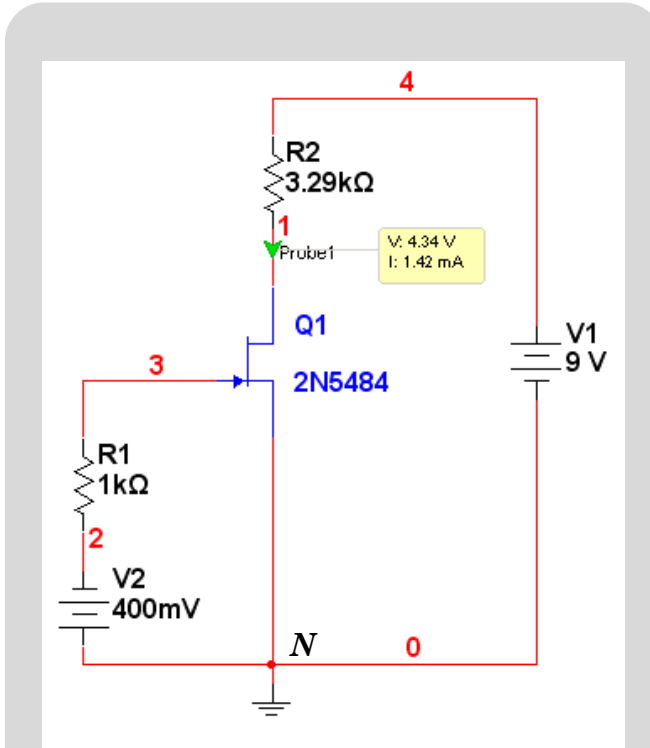
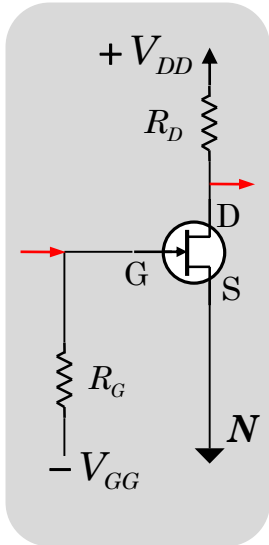
Input: GATE
ac-signal $V_{pp}=20mV$

Output: SOURCE
ac-signal $V_{pp}=20mV$

A biased n-channel JFET CONSTANT VOLTAGE BIAS

Active region

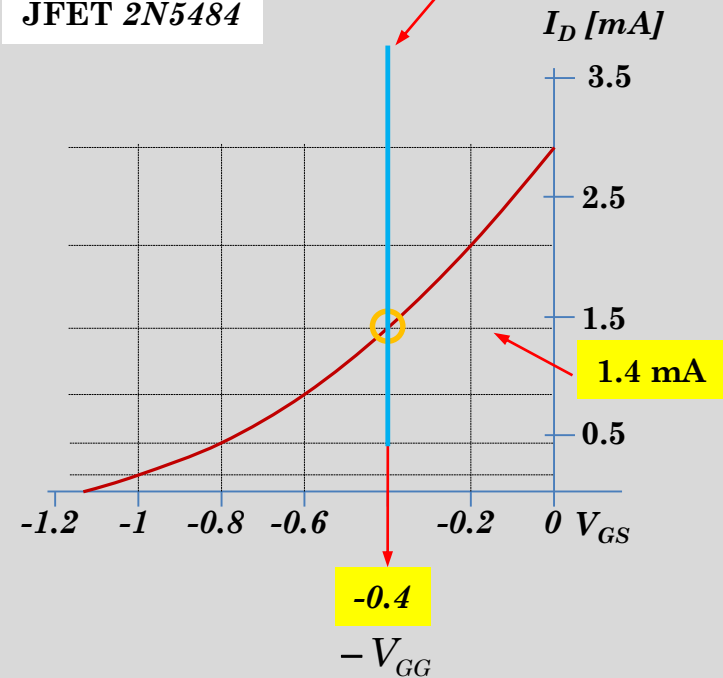
Large signal analysis



DRAIN VOLTAGE $V_{DQ} = 4.34V$
DRAIN CURRENT $I_{DQ} = 1.42mA$

Bias dc LOAD LINE

JFET 2N5484



Q-Point Stability of a biased n-channel JFET

Active region

Large signal analysis

The transfer characteristic of JFET can differ considerably from one device to another of same type.

Electrical Characteristics

TA = 25°C unless otherwise noted

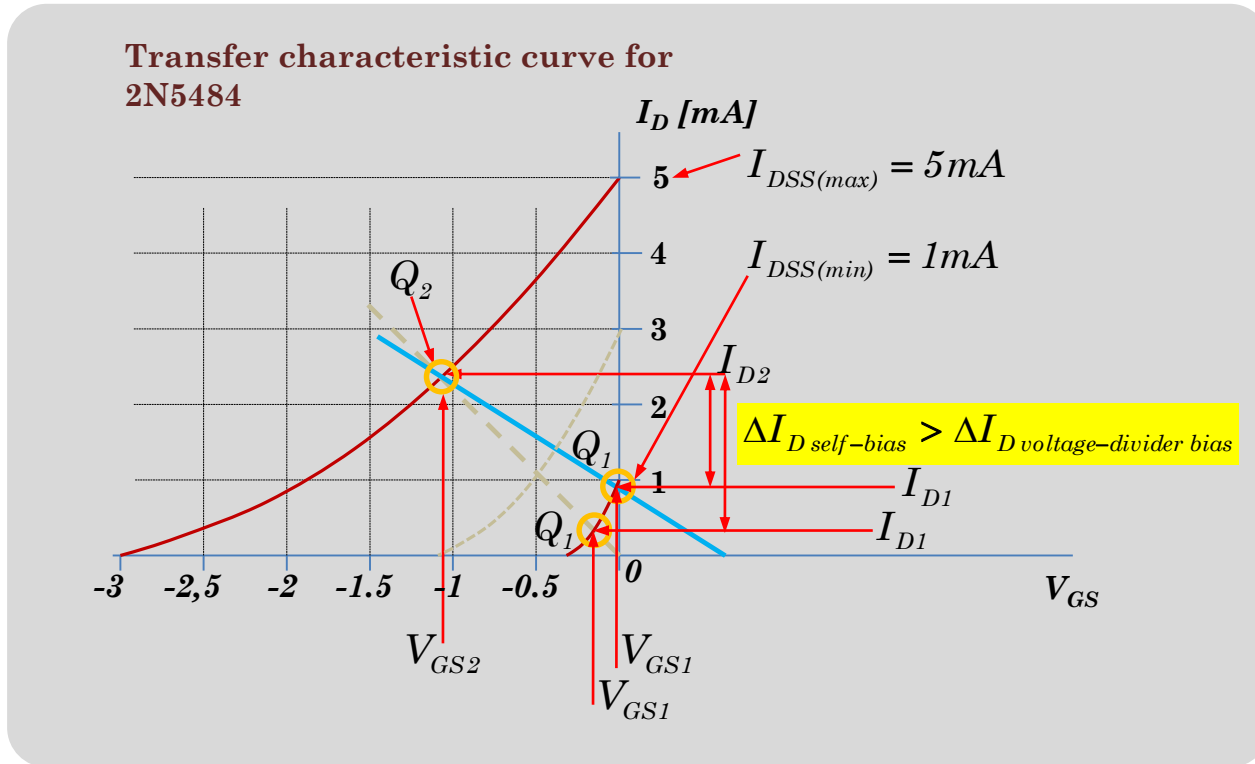
Symbol	Parameter	Test Conditions	Min	Typ	Max	Units
OFF CHARACTERISTICS						
$V_{(BR)GSS}$	Gate-Source Breakdown Voltage	$I_G = -1.0 \mu A, V_{DS} = 0$	-25			V
I_{GSS}	Gate Reverse Current	$V_{GS} = -20 V, V_{DS} = 0$ $V_{GS} = -20 V, V_{DS} = 0, T_A = 100^\circ C$			-1.0 -0.2	nA μA
$V_{GS(off)}$	Gate-Source Cutoff Voltage	$V_{DS} = 15 V, I_D = 10 nA$	5484 5485 5486	-0.3 -0.5 -2.0	-3.0 -4.0 -6.0	V V V
ON CHARACTERISTICS						
I_{DSS}	Zero-Gate Voltage Drain Current*	$V_{DS} = 15 V, V_{GS} = 0$	5484 5485 5486	1.0 4.0 8.0	5.0 10 20	mA mA mA


 Datasheet 2N5484

Q-Point Stability of a biased n-channel JFET

Active region

Large signal analysis



The drain current I_{DQ} is much more stable with VOLTAGE-DIVIDER bias.

Q-Point Stability of a biased n-channel JFET SELF-BIAS WITH CURRENT-SOURCE

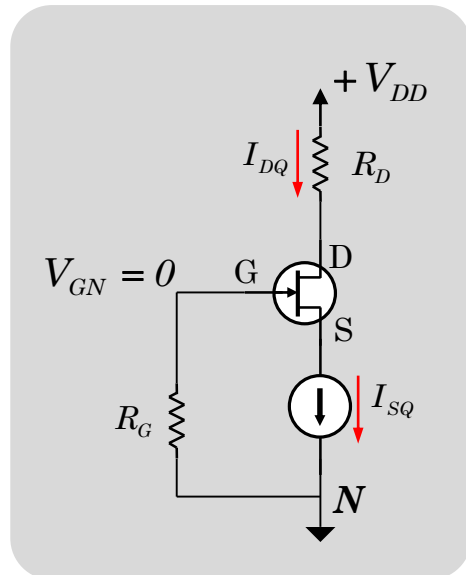
Active region

Large signal analysis

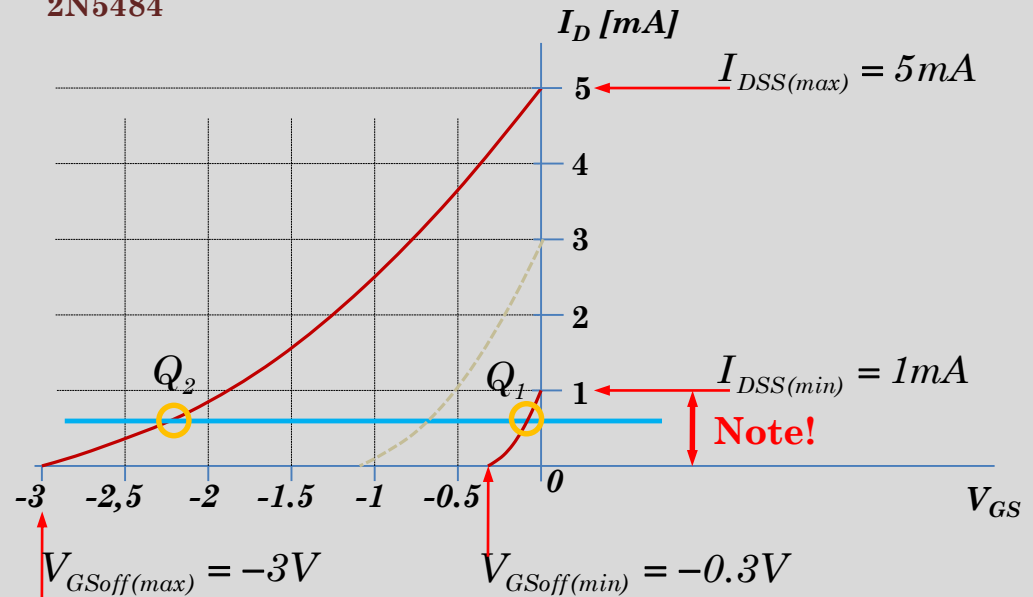
Biasing with the constant-current source.

The drain current I_{DQ} is essentially independent of V_{GS} .

Increased Q-point stability.



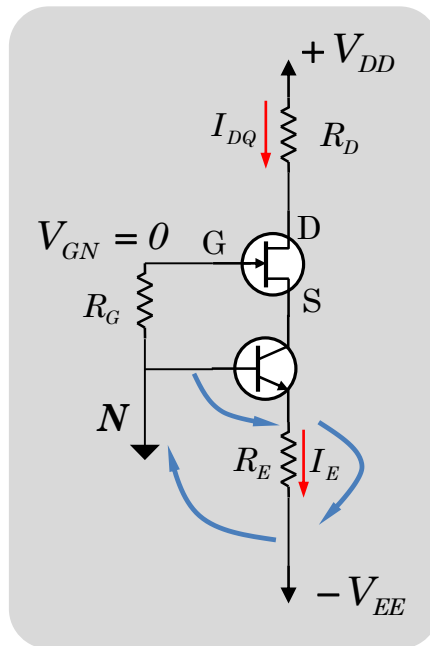
Transfer characteristic curve for
2N5484



Q-Point Stability of a biased n-channel JFET SELF-BIAS WITH CURRENT-SOURCE EXAMPLE

Active region

Large signal analysis



$$-V_{BE} - I_E R_E + V_{EE} = 0$$

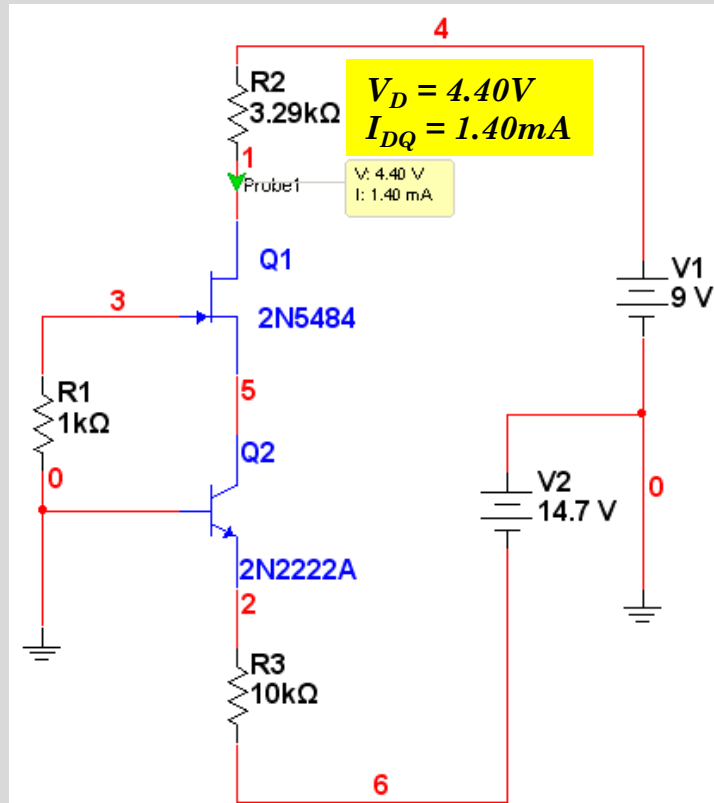
$$V_{EE} \gg V_{BE}$$

$$I_E = \frac{V_{EE} - V_{BE}}{R_E} \approx \frac{V_{EE}}{R_E} \approx I_{DQ}$$

Q-Point Stability of a biased n-channel JFET SELF-BIAS WITH CURRENT-SOURCE EXAMPLE

Active region

Large signal analysis

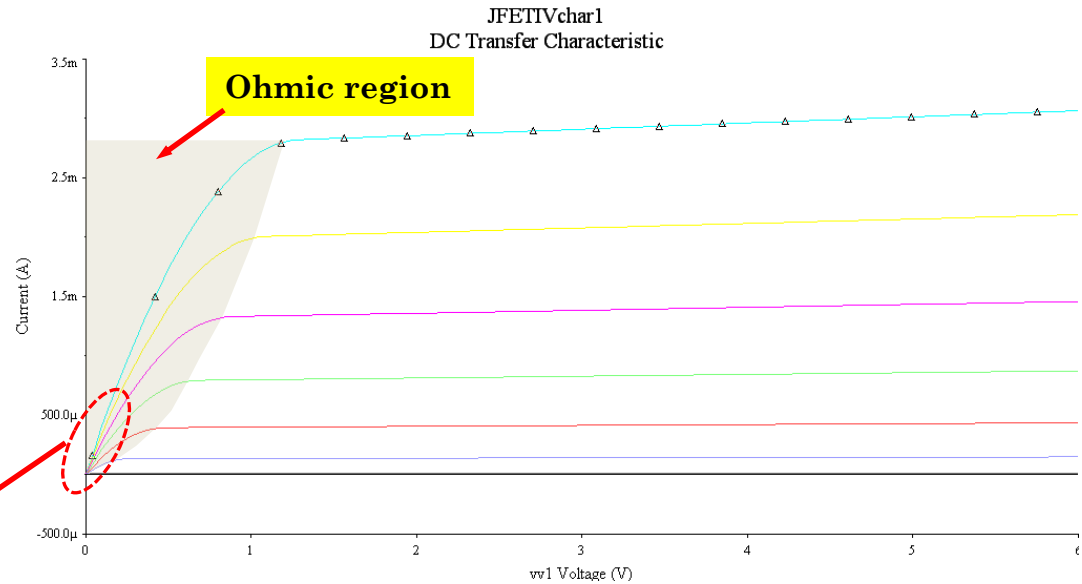
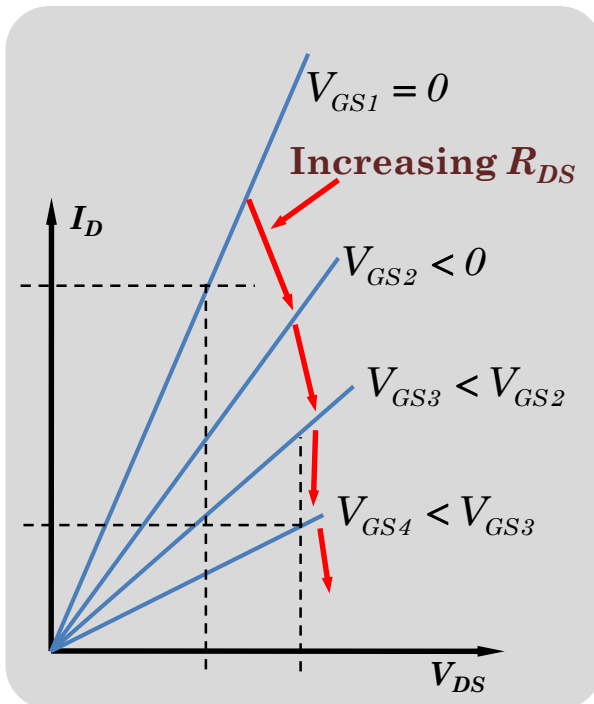


$$I_E = \frac{V_{EE} - V_{BE}}{R_E} = \frac{14.7\text{V} - 0.7\text{V}}{10\text{k}\Omega} = 1.4\text{mA}$$

A biased n-channel JFET

Ohmic region

Large signal analysis



Slope

$$G_{DS} = \frac{I_D}{V_{DS}}$$

$$R_{DS} = \frac{V_{DS}}{I_D} = \frac{1}{G_{DS}}$$

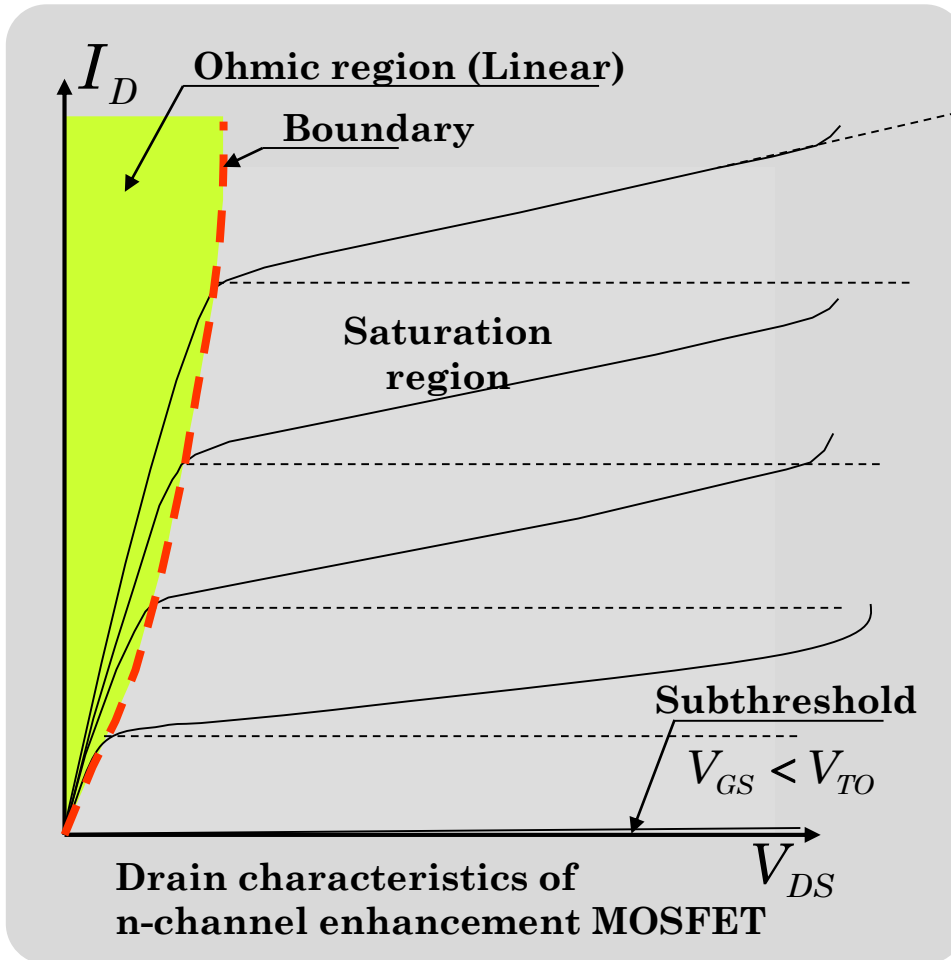
Drain-to-source resistance

Drain-to-source resistance is controlled by V_{GS} .

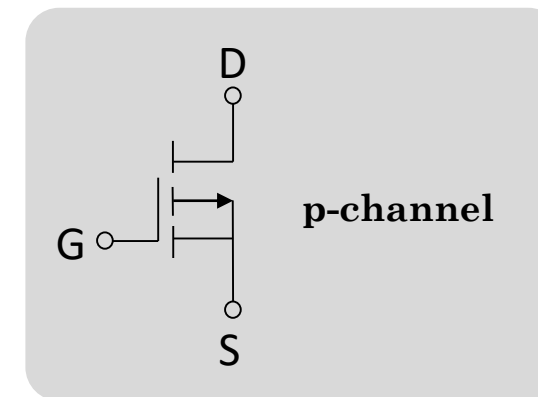
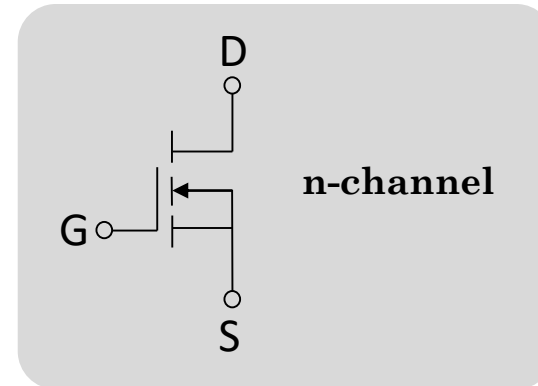
MOSFET (Metal Oxide Semiconductor Field-Effect Transistor)

Large signal analysis

Avaustyyppinen



Drain characteristics with Channel-Length Modulation



MOSFET (Metal Oxide Semiconductor Field-Effect Transistor)

Large signal analysis
Avaustyypinen

Ohmic Region

$$V_{GS} - V_{TO} > V_{DS}$$

$$I_D = k \left(\frac{W}{L} \right) \left[2(V_{GS} - V_{TO})V_{DS} - V_{DS}^2 \right]$$

W/L = aspect ratio

W = channel width

L = channel length

V_{TO} = threshold voltage

k = process parameter

Boundary Region

$$V_{GS} - V_{TO} = V_{DS}$$

$$I_D = k \left(\frac{W}{L} \right) V_{DS}^2$$

$$k = \frac{1}{2} \mu_n C_0$$

μ_n = electron mobility

C_0 = gate capacitance per unit area $fF/\mu m^2$

Saturation Region

$$V_{GS} - V_{TO} < V_{DS}$$

$$I_{DS} = k \left(\frac{W}{L} \right) (V_{GS} - V_{TO})^2 (1 + \lambda V_{DS})$$

Typical values of parameter k

$$10 \text{ to } 50 \mu A/V^2$$

Early voltage = $1/\lambda$

MOSFET (Metal Oxide Semiconductor Field-Effect Transistor)

SPICE MODEL
(large signal)

Ohmic Region $V_{GS} - V_{TO} > V_{DS}$

$$I_D = \frac{KP}{2} \left(\frac{W}{L} \right) \left[2(V_{GS} - V_{TO})V_{DS} - V_{DS}^2 \right]$$

Saturation Region $V_{GS} - V_{TO} < V_{DS}$

$$I_{DS} = \frac{KP}{2} \left(\frac{W}{L} \right) (V_{GS} - V_{TO})^2$$

Saturation Region with channel-length modulation

$$I_{DS} = \frac{KP}{2} \left(\frac{W}{L} \right) (V_{GS} - V_{TO})^2 (1 + \lambda V_{DS})$$

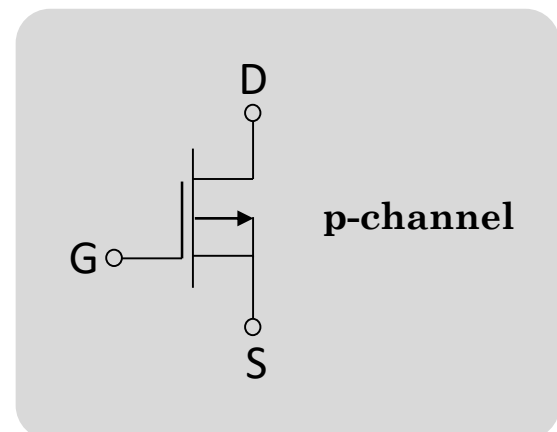
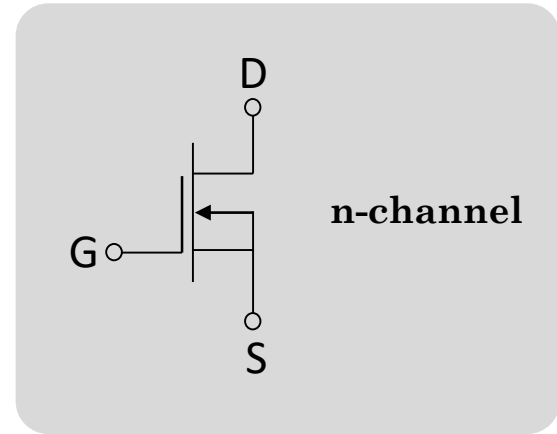
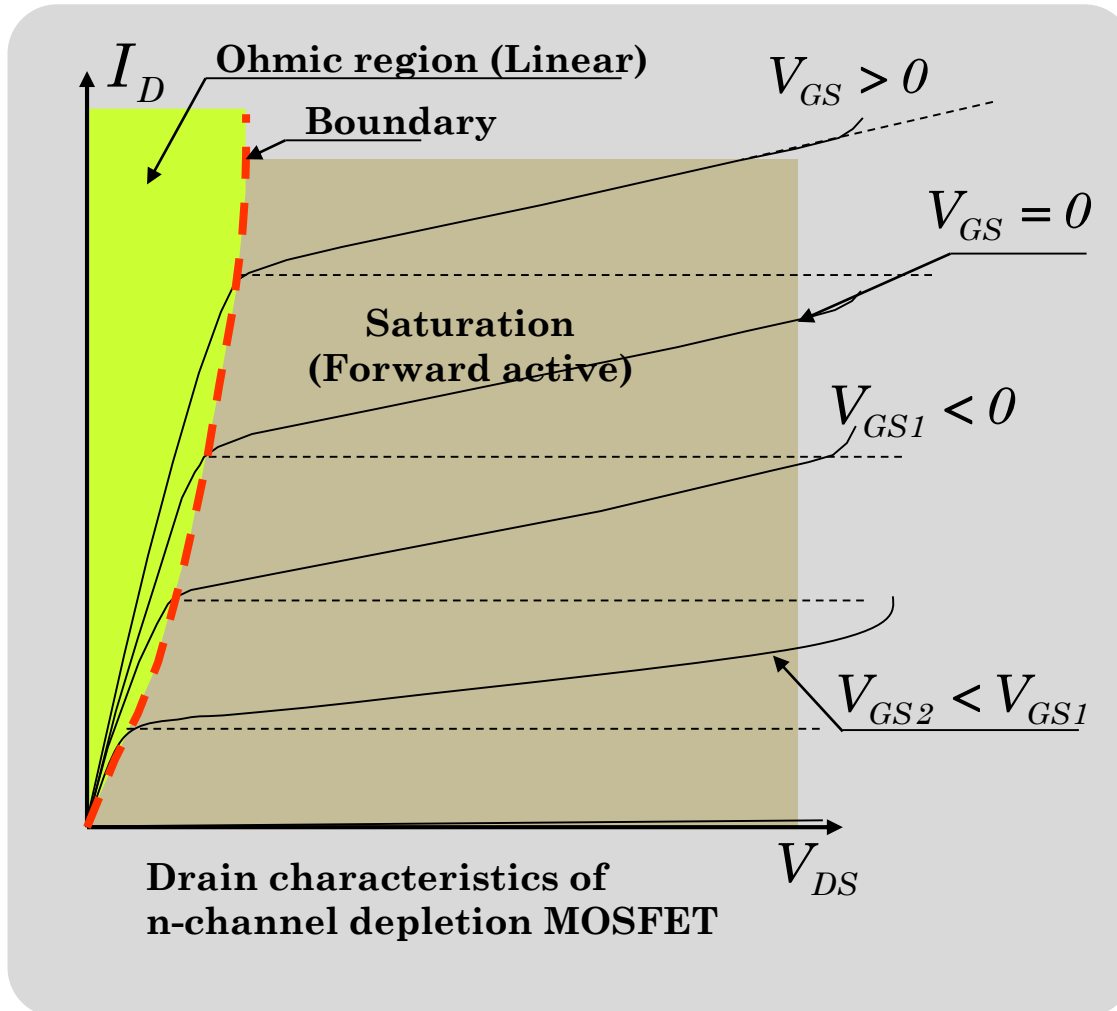
$$KP = \mu_n C_0$$

Typical values :

$$V_{TO} = 0.7V \quad KP = 30 \mu A/V^2$$

MOSFET (Metal Oxide Semiconductor Field-Effect Transistor)

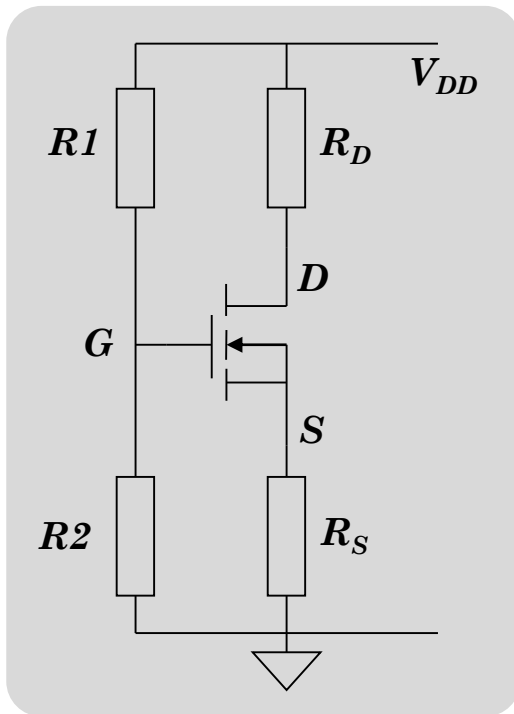
Large signal analysis
Sulkutyypinen



Biasing MOSFET EXAMPLE

Large signal analysis
Avaustyyppinen

Assumption: Early Voltage is very high, $\lambda=0$

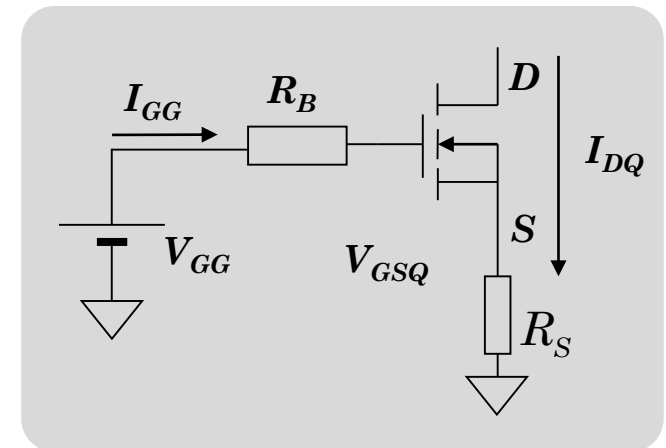


$$KP = 30 \mu\text{A}/\text{V}^2 \quad W/L = 1 \quad I_{GG} = 0$$

Bias point in the Saturation Region $V_{GS} - V_{TO} < V_{DS}$

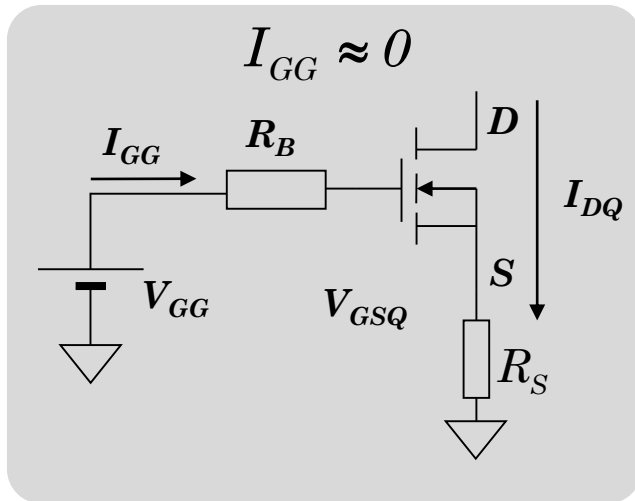
$$R_S = 820 \Omega \quad R_1 \parallel R_2 = 100 \text{ k}\Omega = R_B$$

$$V_{DD} = 12\text{V}$$



Biasing MOSFET EXAMPLE

Large signal analysis
Avaustyypinen



$$\left| \begin{aligned} I_{DQ} &= \frac{KP}{2} \left(\frac{W}{L} \right) (V_{GSQ} - V_{TO})^2 = 420 \mu A \\ V_{GG} - V_{GSQ} - I_{DQ} R_S &= 0 \end{aligned} \right|$$

$$\Rightarrow I_{DQ} = K \left[(V_{GG} - I_{DQ} R_S) - V_{TO} \right]^2$$

$$\text{Where } K = \frac{KP}{2} = 15 \mu A/V^2$$

$$KV_{GG}^2 - 2K(V_{TO} + I_{DQ} R_S)V_{GG} + K(V_{TO} + I_{DQ} R_S)^2 - I_{DQ} = 0$$

$$\Rightarrow V_{GG} = V_{TO} + I_{DQ} R_S \pm \sqrt{\frac{I_{DQ}}{K}} \approx 6.34V$$

Biasing MOSFET EXAMPLE

Large signal analysis
Avaustyyppinen

$$R_1 \parallel R_2 = 100 \text{ k}\Omega = R_B$$

$$V_{GG} = \frac{1}{R_1} (R_1 \parallel R_2) V_{DD}$$

$$R_1 = \frac{V_{DD}}{V_{GG}} R_B = 189.4 \text{ k}\Omega$$

$$R_2 = \frac{R_B R_1}{R_1 - R_B} = 212 \text{ k}\Omega$$

$$V_{GG} - V_{GSQ} - I_{DQ} R_S = 0 \quad \Rightarrow \quad V_{GSQ} = V_{GG} - I_{DQ} R_S \approx 6.0 \text{ V}$$

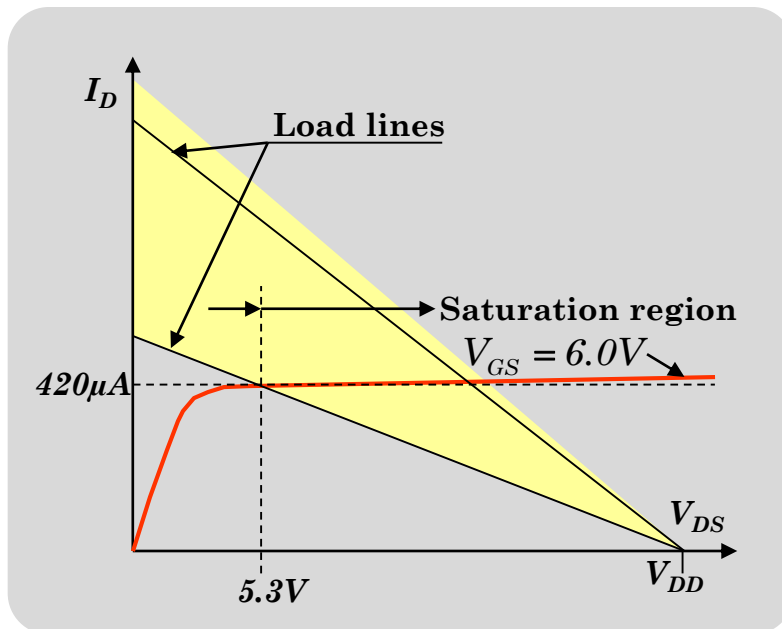
Biasing MOSFET EXAMPLE

Large signal analysis
Avaustyyppinen

Bias point in the Saturation Region $V_{GS} - V_{TO} < V_{DS}$

$$V_{GSQ} - V_{TO} = 6.0V - 0.7V = 5.3V < V_{DS}$$

MOSFET stays in the **saturation region** if $V_{DSQ} > 5.3V$ when $I_{DQ} = 420\mu A$

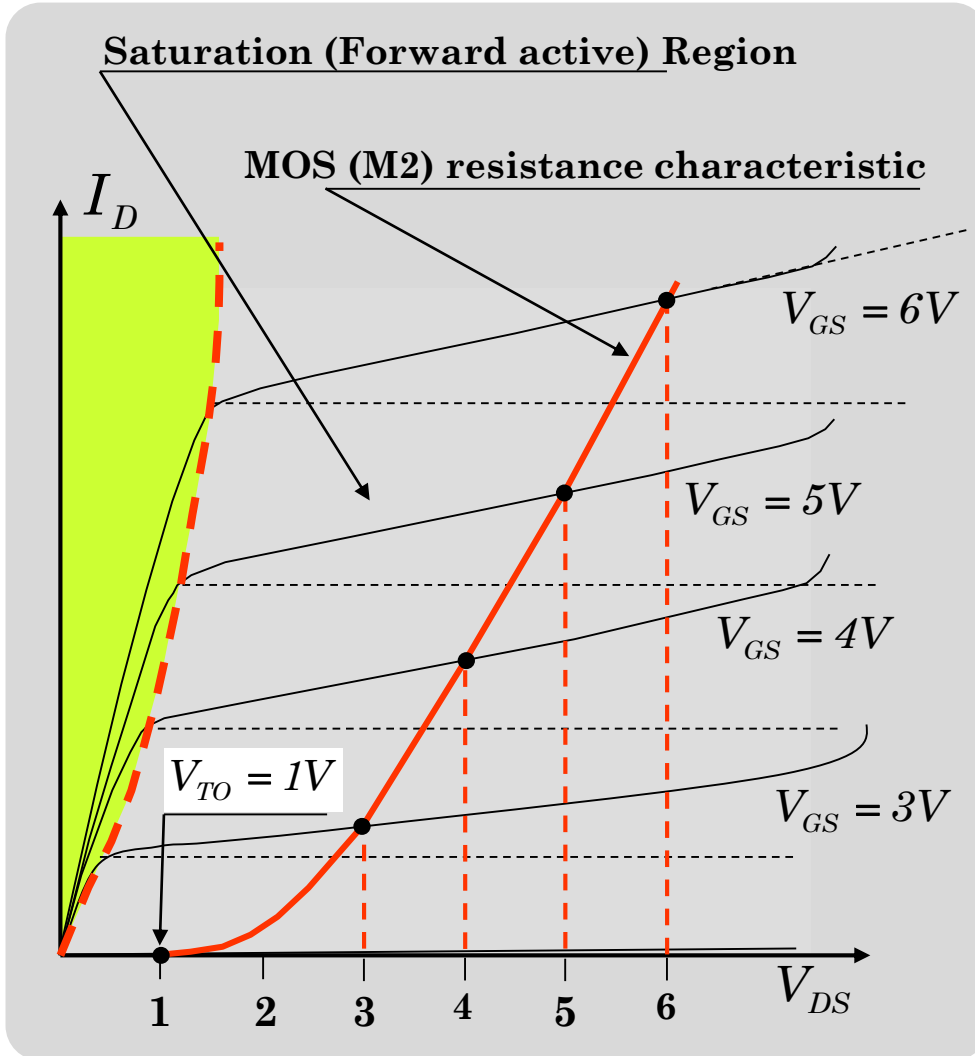


$$V_{DD} - I_{DQ}R_D - V_{DSQ} - I_{DQ}R_S = 0$$

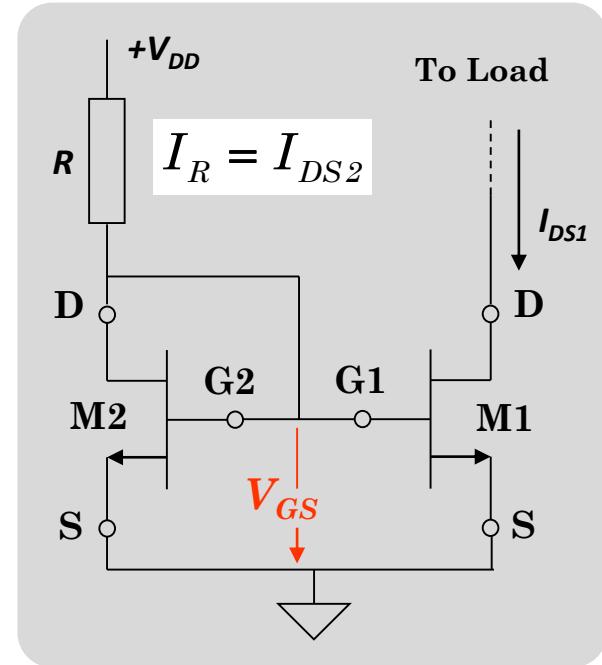
\Rightarrow

$$R_D < 15k\Omega$$

Identical MOSFETS



Large signal analysis



$$V_{DS2} = V_{GS2} \quad V_{GS1} = V_{GS2}$$

Identical FETS $\Rightarrow I_{DS1} = I_{DS2}$

Different MOSFETS

Large signal analysis

$$V_{DS2} = V_{GS2} \quad V_{GS1} = V_{GS2}$$

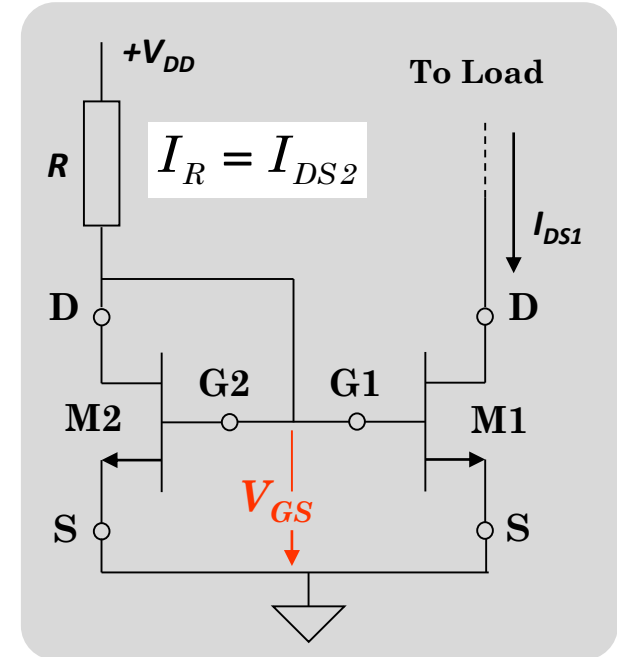
$$M_2 \neq M_1$$

$$\frac{W_2}{L_2} \neq \frac{W_1}{L_1}$$

Different MOSFETS



$$\frac{I_{DS2}}{I_{DS1}} = \frac{(W/L)_2}{(W/L)_1}$$



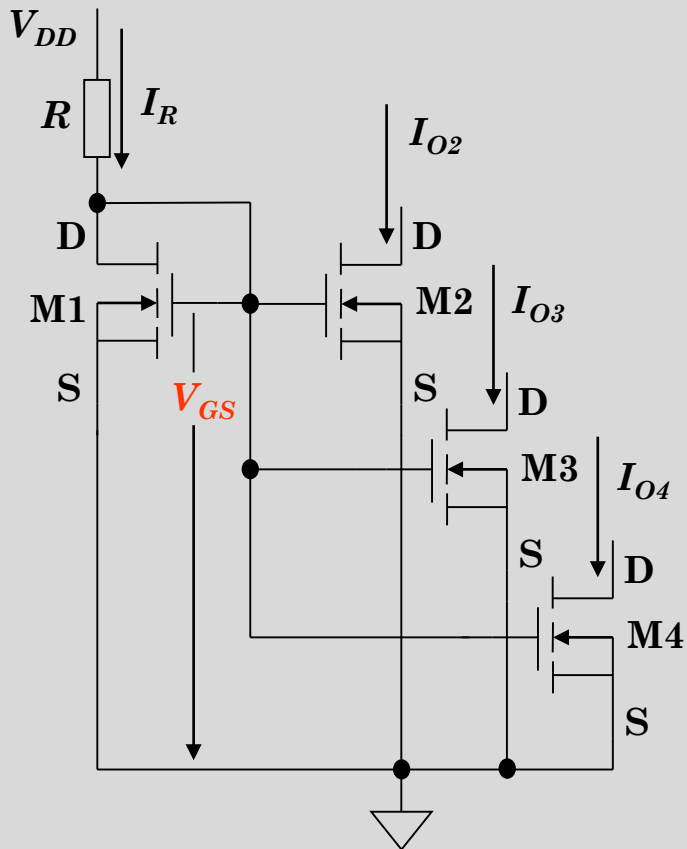
Assumption : $\lambda = 0$

$$V_{GS} = V_{TO} - \frac{1}{2RK} \pm \sqrt{\left(\frac{1}{2RK} - V_{TO}\right)^2 - \left(V_{TO}^2 - \frac{V_{DD}}{RK}\right)}$$

$$I_{DS2} = K(V_{GS} - V_{TO})^2 \quad \text{where} \quad K = \left(\frac{W_2}{L_2}\right) \frac{KP}{2} \quad (\text{MOSFET } M_2)$$

Different MOSFETS

Large signal analysis



$$V_{GS} = V_{TO} - \frac{1}{2RK} \pm \sqrt{\left(\frac{1}{2RK} - V_{TO}\right)^2 - \left(V_{TO}^2 - \frac{V_{DD}}{RK}\right)}$$

(MOSFET M1)

$$I_{DS1} = K(V_{GS} - V_{TO})^2 \quad K = \left(\frac{W_1}{L_1}\right) \frac{KP}{2}$$

$$\frac{I_{O2}}{I_{DS1}} = \frac{W_2/L_2}{W_1/L_1}$$

$$\frac{I_{O3}}{I_{DS1}} = \frac{W_3/L_3}{W_1/L_1}$$

$$\frac{I_{O4}}{I_{DS1}} = \frac{W_4/L_4}{W_1/L_1}$$

The End of Part 4